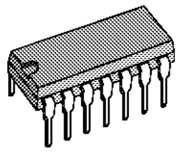
SGS-THOMSON MICROELECTRONICS

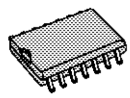
LS404

HIGH PERFORMANCE QUAD OPERATIONAL AMPLIFIERS

- SINGLE OR SPLIT SUPPLY OPERATION
- LOW POWER CONSUMPTION
- SHORT CIRCUIT PROTECTION
- LOW DISTORTION, LOW NOISE
- HIGH GAIN-BANDWIDTH PRODUCT
- HIGH CHANNEL SEPARATION



N
DIP14
(Plastic Package)



D
SO14
(Plastic Micropackage)

DESCRIPTION

The LS404 is a high performance quad operational amplifier with frequency and phase compensation built into the chip. The internal phase compensation allows stable operation as voltage follower in spite of its high gain-bandwidth products.

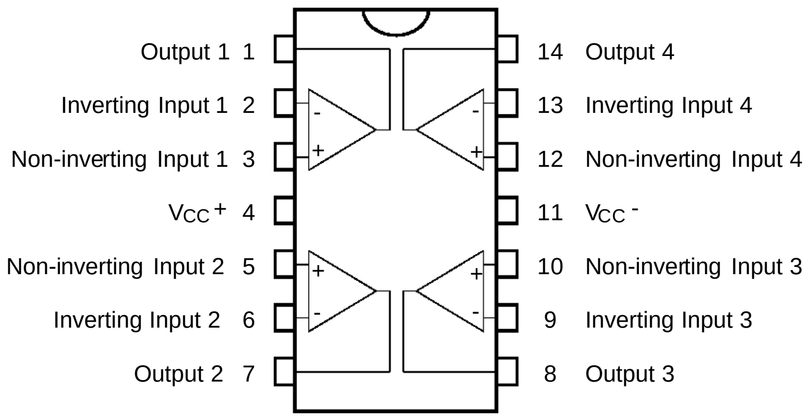
The circuit presents very stable electrical characteristics over the entire supply voltage range, and it particularly intended for professional and telecom applications (active filters, etc).

The patented input stage circuit allows small input signal swings below the negative supply voltage and prevents phase inversion when the inputs is over driver.

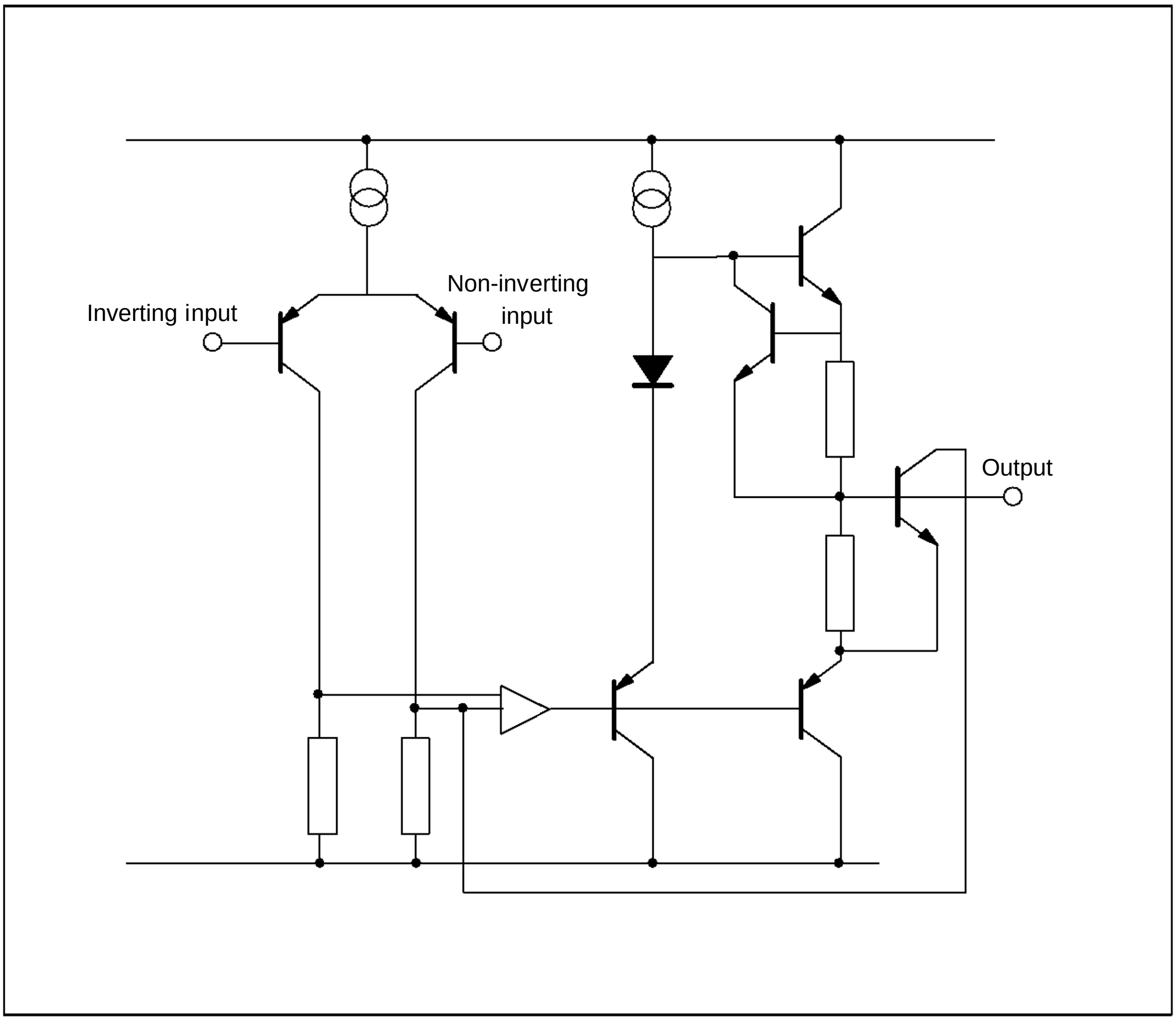
ORDER CODES

Part Number	Temperature Range	Package	
		N	D
LS404C	0°C, +70°C	•	•
LS404I	-40°C, +105°C	•	•
LS404M	-55°C, +125°C	•	•

PIN CONNECTIONS (top view)



EQUIVALENT SCHEMATIC DIAGRAM (1/4 LS404)



ABSOLUTE MAXIMUM RATINGS

Symbol	Parameter		Value	Unit
V_{CC}	Supply Voltage		±18	V
V_i	Input Voltage	(positive) (negative)	$+V_{CC}$ $-V_{CC}$ - 0.5	V
V_{id}	Differential Input Voltage		± (V_{CC} - 1)	
T_{oper}	Operating Temperature Range	LS404C LS404I LS404M	0 to +70 -40 to +105 -55 to +125	°C
P_{tot}	Power Dissipation at T_{amb} = 70°C		400	mW
T_{stg}	Storage Temperature		-65 to 150	°C

ELECTRICAL CHARACTERISTICS (V_{CC} = ±15V, T_{amb} = 25°C, unless otherwise specified)

Symbol	Parameter	Test Conditions	LS404I - LS404M			LS404C			Unit
			Min.	Typ.	Max.	Min.	Typ.	Max.	
I_{CC}	Supply Current			1.3	2		1.5	3	mA
I_{ib}	Input Bias Current			50	200		100	300	nA
R_i	Input Resistance	f = 1kHz		1			1		MΩ
V_{io}	Input Offset Voltage	$R_s \le 10k\Omega$		0.7	2.5		0.5	5	mV
DV_{io}	Input Offset Voltage Drift	$R_s \le 10k\Omega$ $T_{min.} < T_{op} < T_{max.}$		5			5		µV/°C
I_{io}	Input Offset Current			10	40		20	80	nA
DI_{io}	Input Offset Current Drift	$T_{min.} < T_{op} < T_{max.}$		0.08			0.1		nA/°C
I_{os}	Output Short Circuit Current			23			23		mA
A_{vd}	Large Signal Voltage Gain	R_L = 2kΩ V_{CC} = ±15V V_{CC} = ±4V	90	100 95		86	100 95		dB
GBP	Gain-bandwidth Product	f = 100kHz R_L = 2k C_L = 100pF	1.8	3		1.5	2.5		MHz
e_n	Equivalent Input Noise Voltage	f = 1kHz R_s = 50Ω R_s = 1kΩ R_s = 10kΩ		8 10 18	15		10 12 20		$\frac{nV}{\sqrt{Hz}}$
THD	Total Harmonic Distortion	Unity Gain R_L = 2kΩ, V_O = 2V_{pp} f = 1kHz f = 20kHz		0.01 0.03	0.4		0.01 0.03		%
±V_{opp}	Output Voltage Swing	R_L = 2kΩ V_{CC} = ±15V V_{CC} = ±4V	±13	±3		±13	±3		V
V_{opp}	Large Signal Voltage Swing	f = 10kHz R_L = 10kΩ R_L = 1kΩ		22 20			22 20		V_{PP}
SR	Slew Rate	Unity Gain, R_L = 2kΩ	0.8	1.5			1		V/µs
CMR	Common Mode Rejection Ratio	V_{ic} = 10V	90	94		80	90		dB
SVR	Supply Voltage Rejection Ratio	V_{ic} = 1V f = 100Hz	90	94		86	90		dB
V_{O1}/V_{O2}	Channel Separation	f = 1kHz	100	120			120		dB

Figure 1: Supply Current versus Supply Voltage

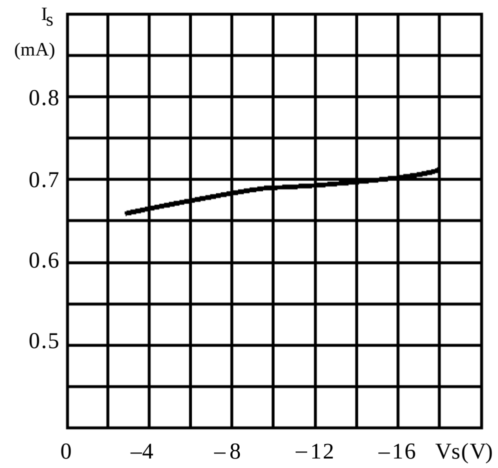


Figure 2 : Supply Current versus Ambient Temperature

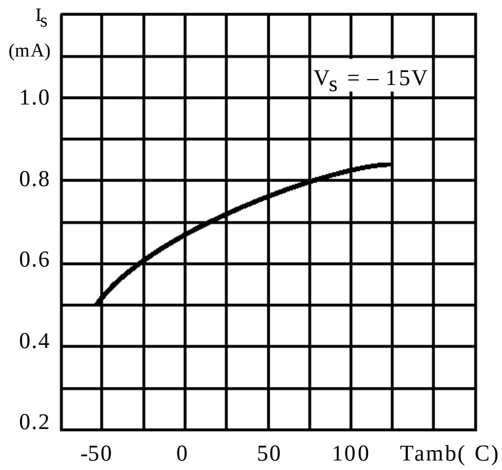


Figure 3 : Output Short Circuit Current versus Ambient Temperature

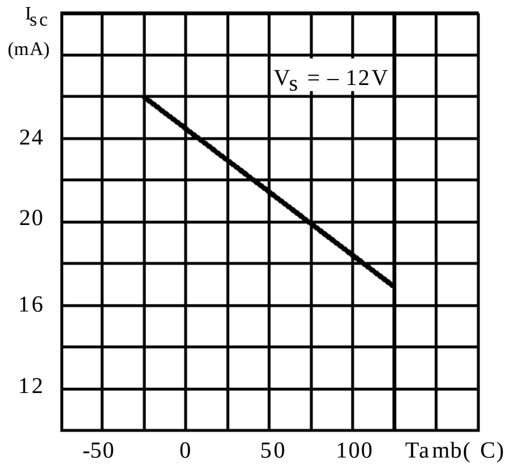


Figure 4 : Open Loop Frequency and Phase Response

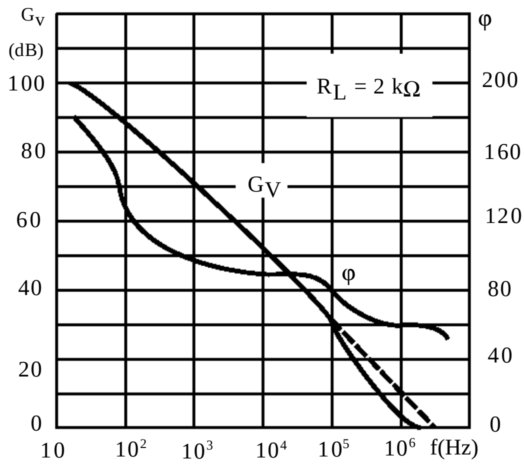


Figure 5 : Output Loop Gain versus Ambient Temperature

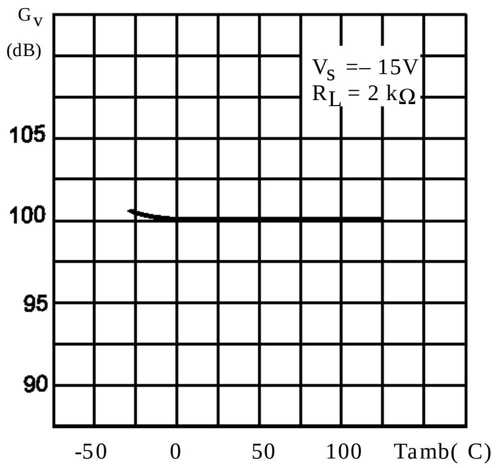


Figure 6 : Supply Voltage Rejection versus Frequency

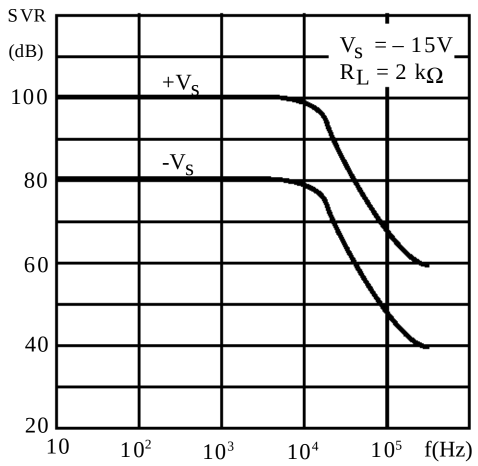


Figure 7: Large Signal Frequency Response

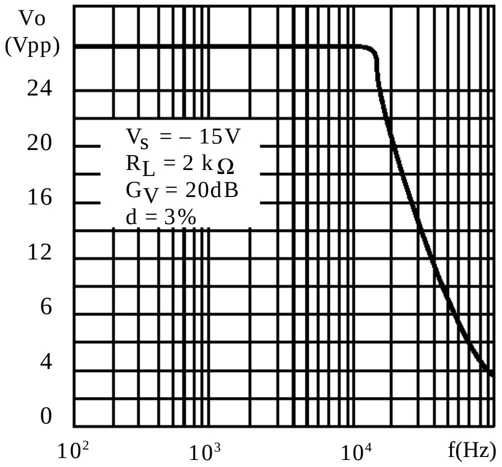


Figure 8 : Output Voltage Swing versus Load Resistance

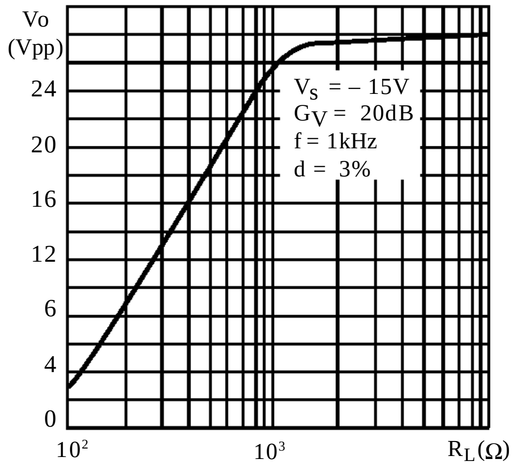


Figure 9 : Total Input Noise versus Frequency

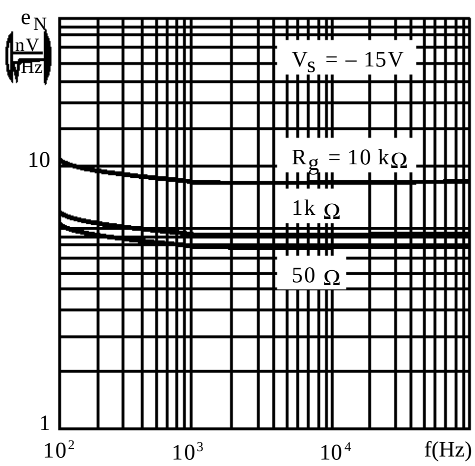


Figure 10 : Amplitude Response

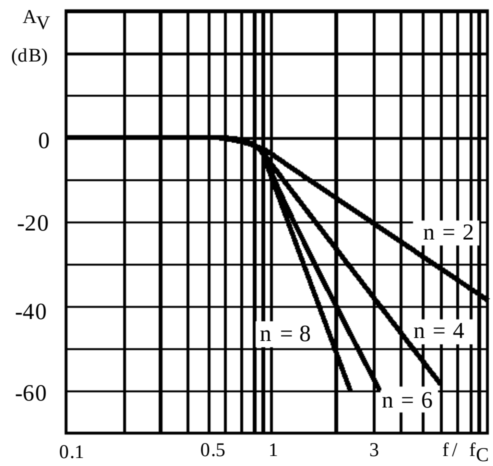


Figure 11 : Amplitude Response

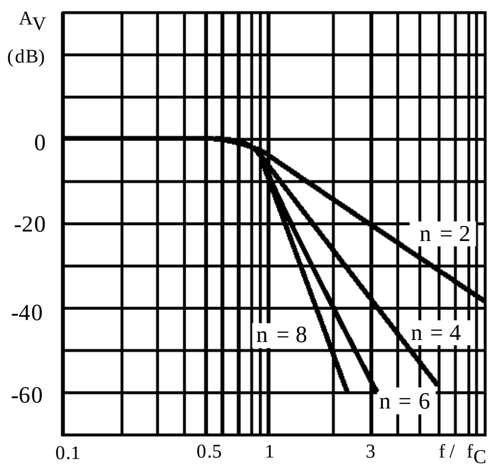
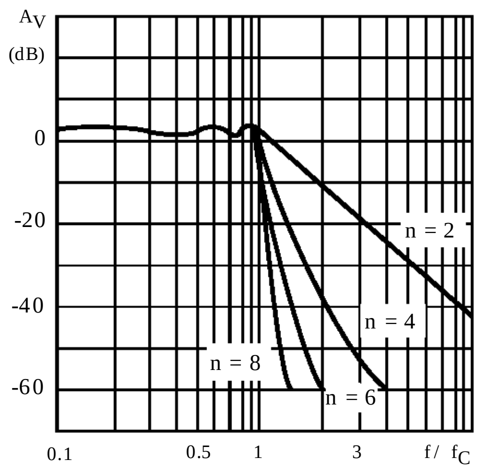


Figure 12 : Amplitude Response (±1dB ripple)



APPLICATION INFORMATION : Active low-pass filter

BUTTERWORTH

The Butterworth is a "maximally flat" amplitude response filter. Butterworth filters are used for filtering signals in data acquisition systems to prevent aliasing errors in sampled-data applications and for general purpose low-pass filtering.

The cut-off frequency f_c, is the frequency at which the amplitude response is down 3dB. The attenuation rate beyond the cutoff frequency is -n6 dB per octave of frequency where n is the order (number of poles) of the filter.

Other characteristics :

- Flattest possible amplitude response.
- Excellent gain accuracy at low frequency end of passband.

BESSEL

The Bessel is a type of "linear phase" filter. Because of their linear phase characteristics, these filters approximate a constant time delay over a limited frequency range. Bessel filters pass transient waveforms with a minimum of distortion. They are also used to provide time delays for low pass filtering of modulated waveforms and as a "running average" type filter.

The maximum phase shift is $\frac{\pm n\Pi}{2}$ radians where n is the order (number of poles) of the filter. The cut-off frequency fc, is defined as the frequency at which the phase shift is one half of this value. For accurate delay, the cut-off frequency should be twice the maximum signal frequency.

The following table can be used to obtain the -3dB frequency of the filter.

	2 pole	4 Pole	6 Pole	8 Pole
–3dB Frequency	$0.77f_c$	$0.67f_c$	$0.57f_c$	$0.50f_c$

Other characteristics :

- Selectivity not as great as Chebyschev or Butterworth.
- Very little overshoot response to step inputs.
- Fast rise time.

CHEBYSCHEV

Chebyschev filters have greater selectivity than either Bessel or Butterworth at the expense of ripple in the passband.

Chebyschev filters are normally designed with peak-to-peak ripple values from 0.2dB to 2dB.

Increased ripple in the passband allows increased attenuation above the cut-off frequency.

The cut-off frequency is defined as the frequency at which the amplitude response passes through the specified maximum ripple band and enters the stop band.

Other characteristics :

- Greater selectivity
- Very non-linear phase response
- High overshoot response to step inputs

The table below shows the typical overshoot and settling time response of the low pass filters to a step input.

	Number of Poles	Peak Overshoot	Settling Time (% of final value)		
		% Overshoot	±1%	±0 .1%	±0 0.1%
Butterworth	2	4	$1.1/f_c$sec.	$1.7/f_c$sec.	$1.9/f_c$sec.
	4	11	$1.7/f_c$	$2.8/f_c$	$3.8/f_c$
	6	14	$2.4/f_c$	$3.9/f_c$	$5.0/f_c$
	8	16	$3.1/f_c$	$5.1/f_c$	$7.1/f_c$
Bessel	2	0.4	$0.8/f_c$	$1.4/f_c$	$1.7/f_c$
	4	0.8	$1.0/f_c$	$1.8/f_c$	$2.4/f_c$
	6	0.6	$1.3/f_c$	$2.1/f_c$	$2.7/f_c$
	8	0.3	$1.6/f_c$	$2.3/f_c$	$3.2/f_c$
Chebyschev (ripple ±0.25dB)	2	11	$1.1/f_c$	$1.6/f_c$	–
	4	18	$3.0/f_c$	$5.4/f_c$	–
	6	21	$5.9/f_c$	$10.4/f_c$	–
	8	23	$8.4/f_c$	$16.4/f_c$	–
Chebyschev (ripple ±1dB)	2	21	$1.6/f_c$	$2.7/f_c$	–
	4	28	$4.8/f_c$	$8.4/f_c$	–
	6	32	$8.2/f_c$	$16.3/f_c$	–
	8	34	$11.6/f_c$	$24.8/f_c$	–

Design of 2nd order active low pass filter (Sallen and Key configuration unity gain-op-amp)

Fixed R = R1 = R2, we have (see fig. 13).

$$C1 = \frac{1}{R}\,\frac{\xi}{\omega_C}$$

$$C2 = \frac{1}{R}\,\frac{1}{\xi\omega_C}$$

The diagram of fig.14 shows the amplitude response for different values of damping factor ξ in 2nd order filters.

Figure 13 : Filter Configuration

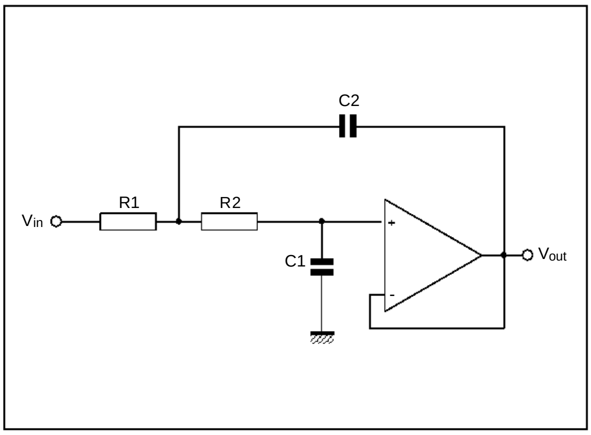
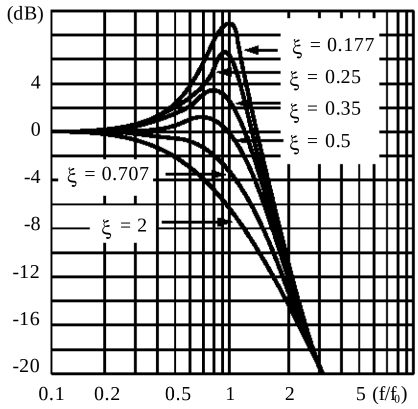


Figure 14 : Filter Respons versus Damping Factor



Three parameters are needed to characterize the frequency and phase response of a 2nd order active filter : the gain (G_V), the damping factor (ξ) or the Q-factor ($Q = (2\,\xi)^{1}$), and the cut-off frequency (f_c).

The higher order responses are obtained with a series of 2nd order sections. A simple RC section is introduced when an odd filter is required.

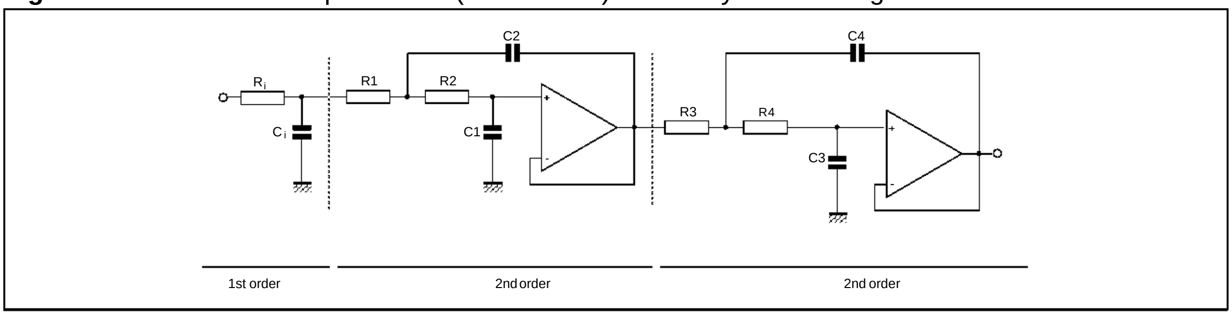
The choice of 'ξ' (or Q-factor) determines the filter response (see table 1).

Table 1

Filter Response	ξ	Q	Cutoff Frequency f_c
Bessel	$\frac{\sqrt{3}}{2}$	$\frac{\sqrt{1}}{3}$	Frequency at which Phase Shift is -90°C
Butterworth	$\frac{\sqrt{2}}{2}$	$\frac{\sqrt{1}}{2}$	Frequency at which G_V = -3dB
Chebyschev	$\frac{\sqrt{2}}{2}$	$\frac{\sqrt{1}}{2}$	Frequency at which the amplitude response passes through specified max. ripple band and enters the stop band.

EXAMPLE

Figure 15 : 5th Order Low-pass Filter (Butterworth) with Unity Gain Configuration



In the circuit of fig. 15, for $f_c = 3.4kHz$ and $R_i = R_1 = R_2 = R_3 = R_4 = 10k\Omega$, we obtain :

$$C_i = 1.354 . \frac{1}{R} . \frac{1}{2\Pi f_C} = 6.33nF$$

$$C_1 = 0.421 . \frac{1}{R} . \frac{1}{2\Pi f_C} = 1.97nF$$

$$C_2 = 1.753 . \frac{1}{R} . \frac{1}{2\Pi f_C} = 8.20nF$$

$$C_3 = 0.309 . \frac{1}{R} . \frac{1}{2\Pi f_C} = 1.45nF$$

$$C_4 = 3.325 . \frac{1}{R} . \frac{1}{2\Pi f_C} = 15.14nF$$

The attenuation of the filter is 30dB at 6.8kHz and better than 60dB at 15kHz.

The same method, referring to Tab. 2 and fig. 16, is used to design high-pass filter. In this case the damping factor is found by taking the reciprocal of the numbers in Tab. 2. For $f_c = 5kHz$ and $C_i = C_1 = C_2 = C_3 = C_4 = 1nF$ we obtain :

$$R_i = \frac{1}{0.354} . \frac{1}{C} . \frac{1}{2\Pi f_C} = 25.5k\Omega$$

$$R_1 = \frac{1}{0.421} . \frac{1}{C} . \frac{1}{2\Pi f_C} = 75.6k\Omega$$

$$R_2 = \frac{1}{1.753} . \frac{1}{C} . \frac{1}{2\Pi f_C} = 18.2k\Omega$$

$$R_3 = \frac{1}{0.309} . \frac{1}{C} . \frac{1}{2\Pi f_C} = 103k\Omega$$

$$R_4 = \frac{1}{3.325} . \frac{1}{C} . \frac{1}{2\Pi f_C} = 9.6k\Omega$$

Table 2 : Damping Factor for Low-pass Butterworth Filters

Order	C_i	C_1	C_2	C_3	C_4	C_5	C_6	C_7	C_8
2		0.707	1.41						
3	1.392	0.202	3.54						
4		0.92	1.08	0.38	2.61				
5	1.354	0.421	1.75	0.309	3.235				
6		0.966	1.035	0.707	1.414	0.259	3.86		
7	1.336	0.488	1.53	0.623	1.604	0.222	4.49		
8		0.98	1.02	0.83	1.20	0.556	1.80	0.195	5.125

Figure 16 : 5th Order High-pass Filter (Butterworth) with Unity Gain Configuration

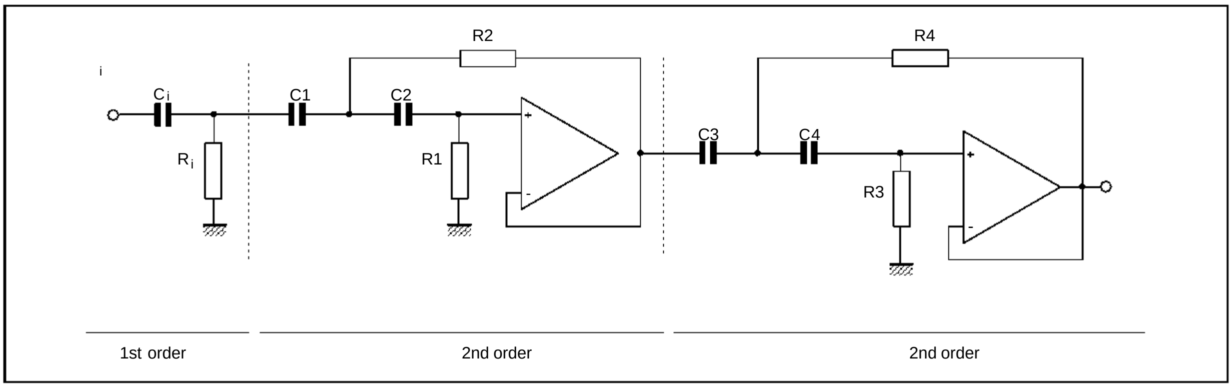


Figure 17 : Mutliple Feedback 8-pole Bandpass Filter

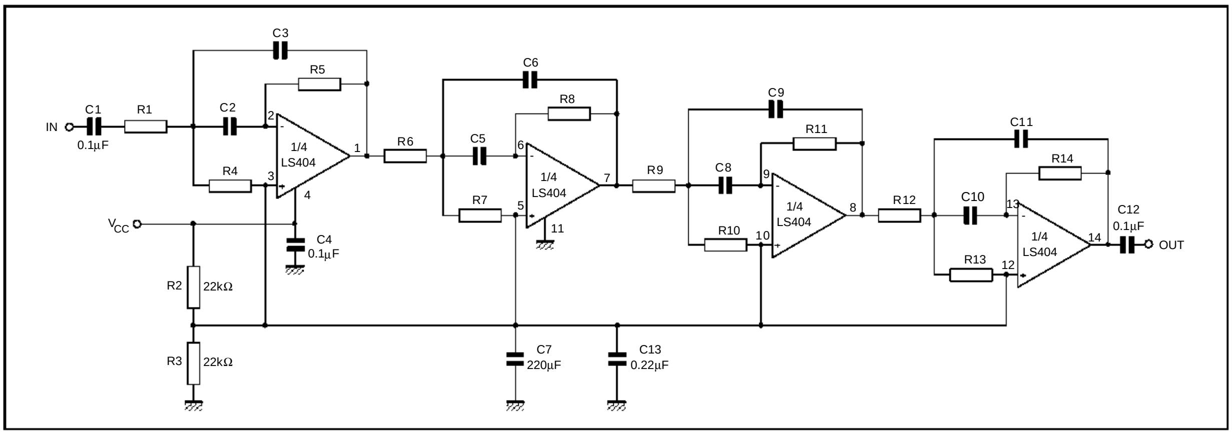


Figure 18 : Frequency Response of Bandpass Filter

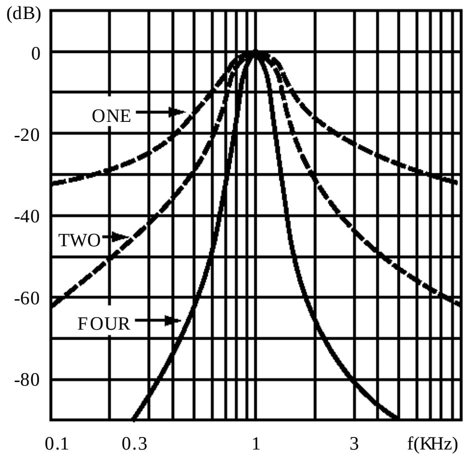


Figure 19 : Bandwidth of Bandpass Filter

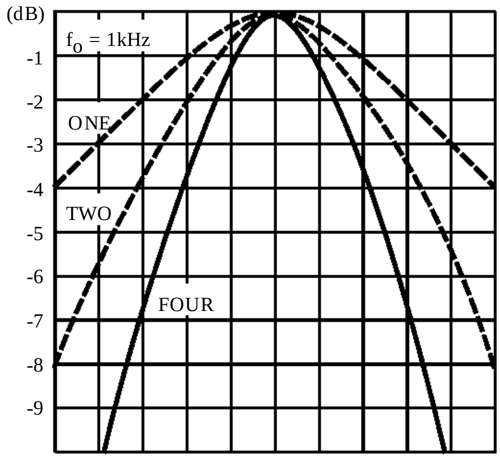
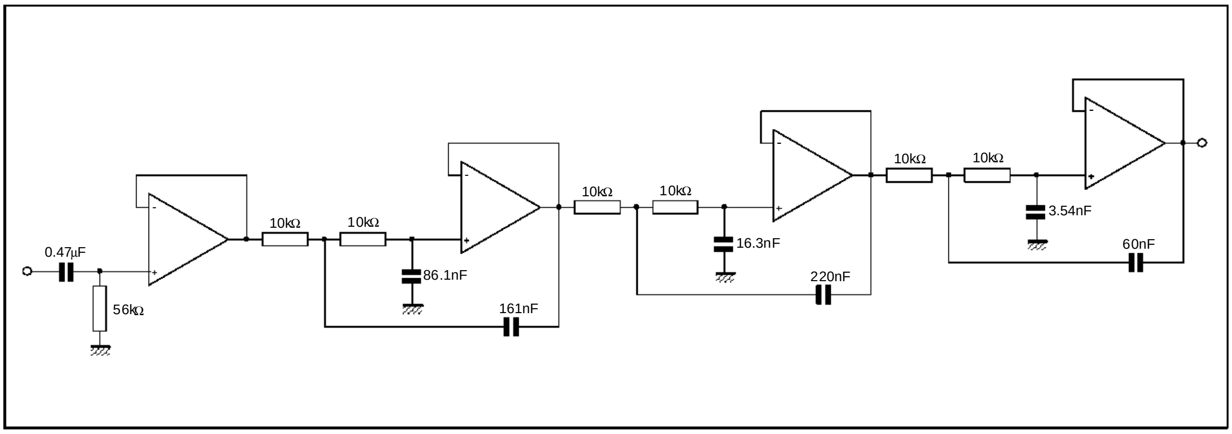
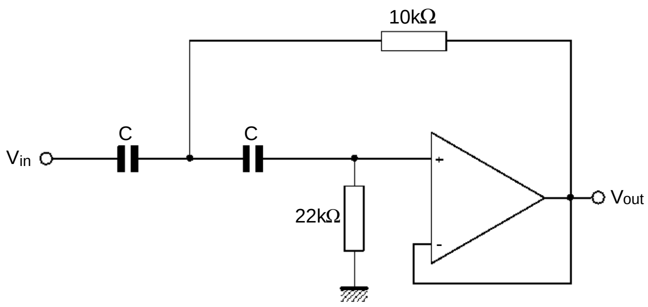


Figure 20 : Six-pole 355Hz Low-pass Filter (chebychev type)



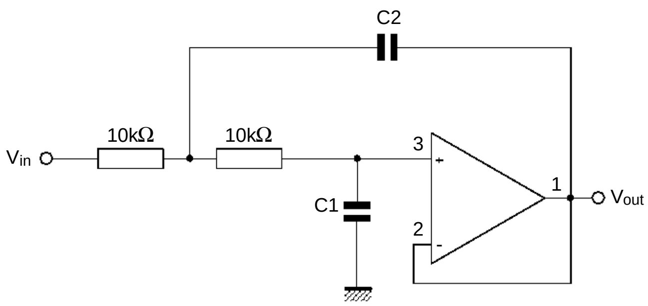
This is a 6-pole Chebychev type with ±0.25dB ripple in the passband. A decoupling stage is used to avoid the influence of the input impedance on the filter's characteristics. The attenuation is about 55dB at 710Hz and reaches 80dB at 1065Hz. The in band attenuation is limited in practise to the ±0.25dB ripple and does not exceed 0.5dB at 0.9fc.

Figure 21 : Subsonic Filter (G_V = 0dB)



f_C (Hz)	C (μF)
15	0.68
22	0.47
30	0.33
55	0.22
100	0.10

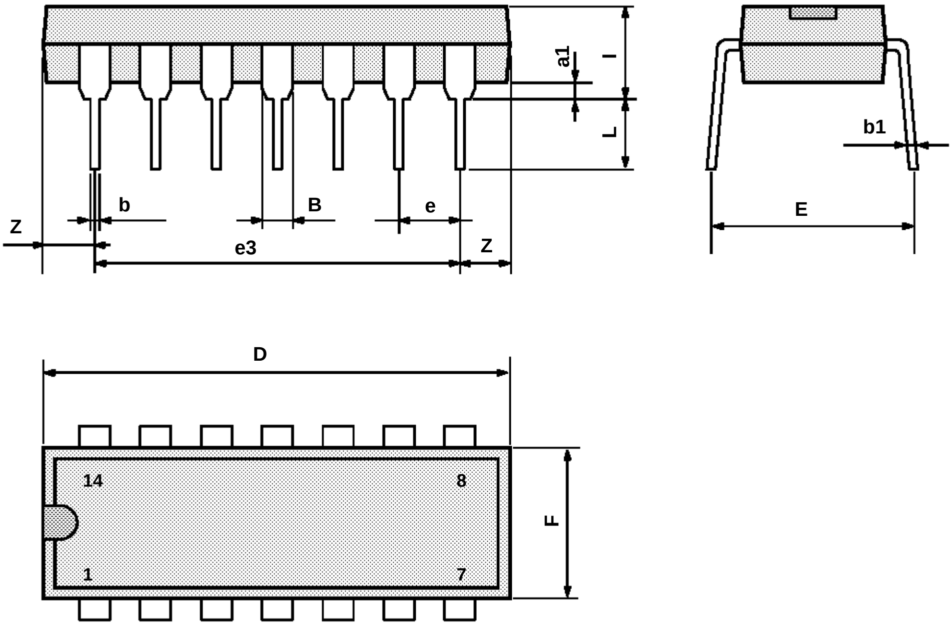
Figure 22 : High Cut Filter (G_V = 0dB)



f_C (Hz)	C1 (nF)	C2 (nF)
3	3.9	6.8
5	2.2	4.7
10	1.2	2.2
15	0.68	1.5

PACKAGE MECHANICAL DATA

14 PINS - PLASTIC DIP



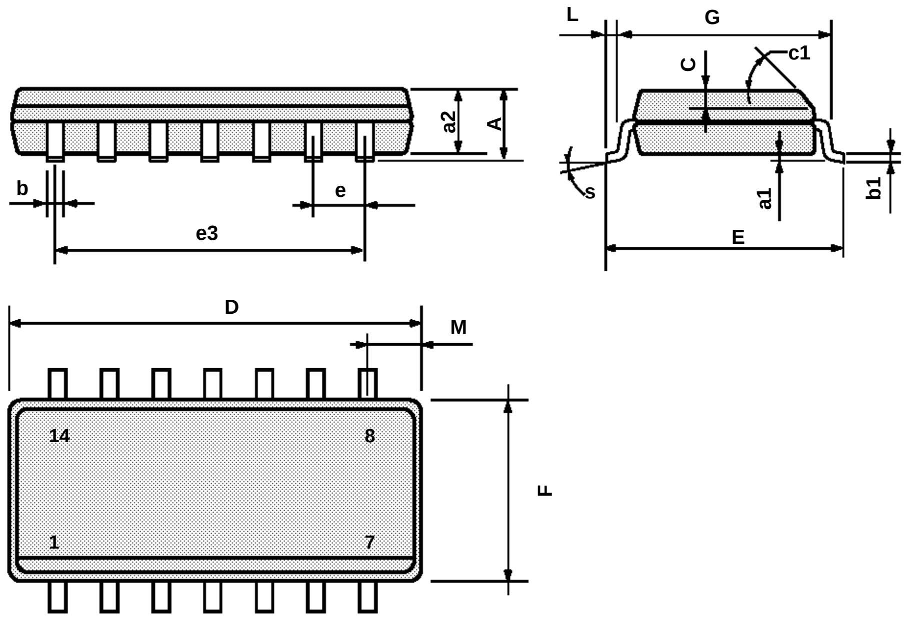
PM-DIP14.EPS

Dimensions	Millimeters			Inches		
	Min.	Typ.	Max.	Min.	Typ.	Max.
a1	0.51			0.020		
B	1.39		1.65	0.055		0.065
b		0.5			0.020	
b1		0.25			0.010	
D			20			0.787
E		8.5			0.335	
e		2.54			0.100	
e3		15.24			0.600	
F			7.1			0.280
i			5.1			0.201
L		3.3			0.130	
Z	1.27		2.54	0.050		0.100

DIP14.TBL

PACKAGE MECHANICAL DATA

14 PINS - PLASTIC MICROPACKAGE (SO)



Dimensions	Millimeters			Inches		
	Min.	Typ.	Max.	Min.	Typ.	Max.
A			1.75			0.069
a1	0.1		0.2	0.004		0.008
a2			1.6			0.063
b	0.35		0.46	0.014		0.018
b1	0.19		0.25	0.007		0.010
C		0.5			0.020	
c1	45^{o} (typ.)					
D	8.55		8.75	0.336		0.334
E	5.8		6.2	0.228		0.244
e		1.27			0.050	
e3		7.62			0.300	
F	3.8		4.0	0.150		0.157
G	4.6		5.3	0.181		0.208
L	0.5		1.27	0.020		0.050
M			0.68			0.027
S	8^{o} (max.)					

SO14.TBL

ORDER CODE :